3-2

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015 Program: B.Sc. Engineering (Civil)

Course Code: IMG 301 Full Marks: 50

5x6

2x10

Section A

(Answer any five Questions)

- 1. Describe the Informal Organization.
- 2. Explain the Disadvantages of Narrow span of management.
- 3. How effectively you can use Grapevine?
- 4. Describe any traditional Need theory.
- 5. Explain the Free-rein Leadership style.
- 6. Write down the Basic Control process.
- 7. Describe the e-commerce options.

Section B

(Answer any two Questions)

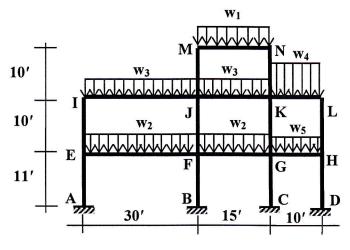
- 8. As a manager, how you can do 'Job Enrichment'?
- 9. Describe a contemporary Need theory of motivation.
- 10. Explain the various types of Communication flow inside the organization.

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015 Program: B.Sc. Engineering (Civil)

Course Code: CE 313	Time: 180 Minutes
Course Title: Structural Engineering II	Full Marks: 20x10 = 200

<u>Answer any 10</u> of the following 14 Questions. (Each question carries equal marks). *The figures are not drawn to scale*.

[1] What are the assumptions for the vertical load analysis of Frames? Draw the approximate Shear Force and Bending Moment Diagram of EF, FG, and KL shown in Figure 1? Given, w₁ = 1.25 k/', w₂ = 2.5 k/', w₃ = 3 k/', w₄ = 8 k/', w₅ = 2 k/'.





[2] Determine the approximate Axial Force, Shear Force and Moment of the following columns AE, BF, CG and DH of the frame shown in Figure 2 by using the Cantilever Method.

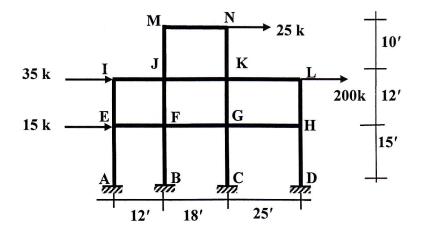
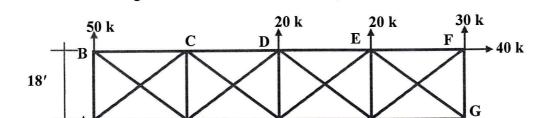


Figure 2



I

J

18'

20 k

18'

[3] Calculate the forces in members **BC**, **AJ** and **DH** of the statically indeterminate truss shown in Figure 3. Consider that the Diagonal members can take tension only.



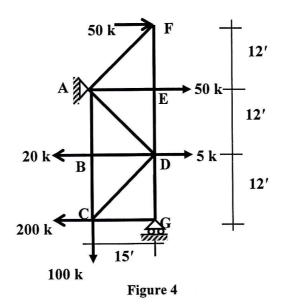
H

18'

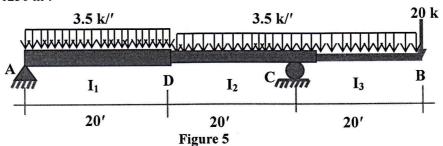
10 k

18'

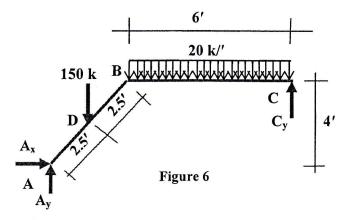
[4] Determine the Horizontal (rightward) and Vertical (downward) deflection of joint D of the truss shown in Figure 4 by using the Virtual Work Method. Consider, $E = 29 \times 10^3$ ksi, truss members area A = 2.5 in² except member AE which has an area of 4 in².



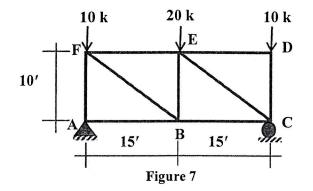
[5] Calculate the rotation (counter clockwise) and vertical (upward) deflection at point B of the beam shown in Figure 5 by using the Virtual Work Method. Consider, $E = 29 \times 10^3$ ksi, $I_1 = 5000$ in⁴, $I_2 = 2500$ in⁴.



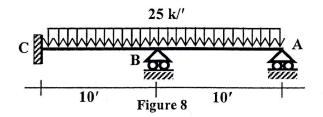
[6] Determine the rotation (counter clockwise) and vertical (downward) deflection at point B of the frame ABC shown in Figure 6 by using the Virtual Work Method. The cross-section of the members are same and assume $E = 25 \times 10^3$ ksi, I = 800 in⁴.



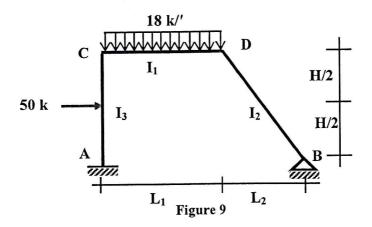
[7] Use the Method of Virtual Work determine the minimum cross-sectional area for the members of the truss shown in Figure 7, so that the vertical deflection at joint B does not exceed 0.5 inches. Assume, E=1.8x10³ksi, EA is constant.



[8] Draw the Bending Moment Diagram of the beam shown in Figure 8 by employing the Flexibility Method. Consider, $E = 45 \times 10^3$ ksi, I = 1800 in⁴.

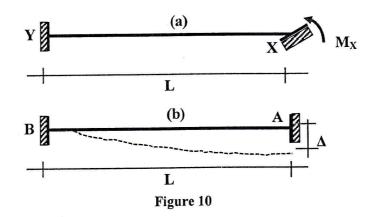


[9] Determine the Support Reactions and draw the Shear and Bending Moment Diagrams of the structure shown in Figure 9 by using the **Method of Consistent Deformations**. Consider, $E = 40 \times 10^3$ ksi, $I_1 = 4000$ in⁴, $I_2 = 3000$ in⁴, $I_3 = 2500$ in⁴, $L_1 = 30'$, $L_2 = 20'$, H = 25'.

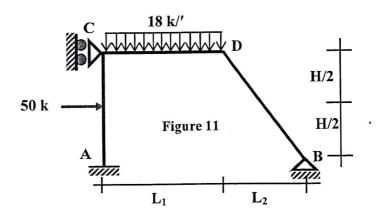


[10] Use the Moment Area Theorem and consider EI is constant for the beam shown in Figure 10.

- (i) For the beam shown in Figure 10 (a) derive the expression, Rotational Stiffness and Moment Carryover Factor. Given, rotation at X is θ .
- (ii) For the beam shown in Figure 10 (b) derive the expression, the Shear Stiffness and Bending Moment at B. Given, vertical deflection at A is Δ .

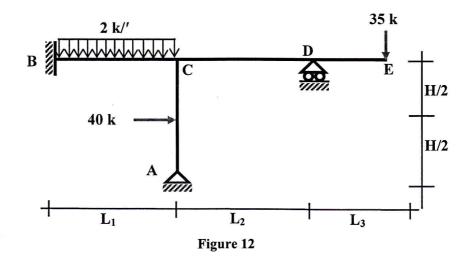


[11] Determine the member end moments and draw the Bending Moment diagram for the frame of Figure 11 for the loading shown in the figure and the support settlements of 1 inch at A by using the Moment₃. Distribution Method. Consider, $E = 48 \times 103$ ksi, I = 1600 in4, $L_1 = 5'$, $L_2 = 3'$, H = 4'.



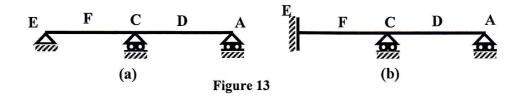
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[12] Determine the member end moments and draw the Bending Moment diagram for the frame of Figure 12 for the loading shown in the figure and the support settlements of 1 inch at A and 1.5 inch at D by using the **Moment Distribution Method**. Consider, $E = 40x10^3$ ksi, I = 4800 in⁴, $L_1 = 30'$, $L_2 = 30'$, $L_3 = 10'$, H = 20'.



[13] Answer the following questions

 (i) What is Influence Line (IL)? Draw the qualitative IL for M_A, V_D and R_C for the beams shown in Figure 13 (a-b).



(ii) Draw the qualitative influence lines of maximum positive moment at E, $M_E^{\max(+)}$ and maximum negative shear at F, $V_F^{\max(-)}$ for the frame shown in Figure 14. Also place the Live Load 25 kN/m and Concentrated Moving Load 50 kN.

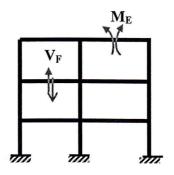


Figure 14

[14] Calculate the member forces and the support reactions of the truss ABCD shown in Figure 15 by using the Flexibility Method. Assume that the $E = 28 \times 10^3$ ksi, area is same for all members A = 4 in².

1

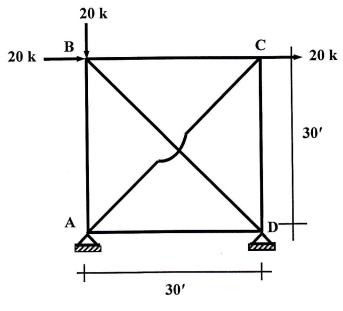


Figure 15

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015

Course Code: CE 317 (A) Course Title: Design of Reinforced Concrete II

Time: 3 (Three) Hours Full Marks: 100

PART A

[There are 10 (ten) questions. Answer any 7 (seven)] (All symbols have their usual meanings. Assume reasonable value for any missing data)

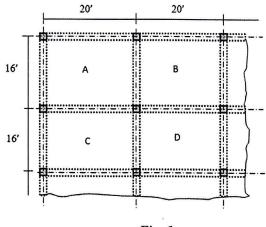
1. A two-way beam supported slab system with columns 22"×22"square inch is shown in Fig:1. The slab contains floor finish of 35 psf, random wall = 50 psf and live load = 75 psf. Determine the following for slab-D.

a. Moment Coefficients: $C_{a(D)+}, C_{a(L)+}, C_{a-}, C_{b(D)+}, C_{b(L)+}$ and C_{b-}

b. Moments: $M_{a+}, M_{a-}, M_{b+}, M_{b-}$

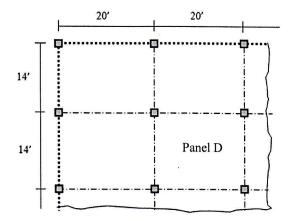
c. Required reinforcements: Asa+, Asa-, Asb+, Asb-

d. Draw reinforcement details in a neat diagram.





Design an interior panel (D) of a flat slab (*Fig: 2*) of size 20'×14'c/c (supported on 12'×12' edge beams), if it carries floor finish = 30 psf, random wall = 50 psf, live load = 60 psf. Given: f_c'= 3 ksi, f_y = 50 ksi.



3. A 12×20 inch column is reinforced with four #9 bars as shown in the *Fig: 3*. Given that $f_c' = 4$ ksi, $f_y = 60$ ksi. Determine:

a. the load P_b, moment M_b and corresponding eccentricity e_b for balanced failure;

b. the load and moment for a point in the tension failure region of the interaction diagram.

c. the load and moment for a point in the compression failure region of the interaction diagram.

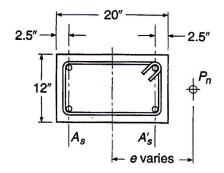


Fig: 3

4. Figure 4 shows the plan of a 6-storied RC structure, with 5" thick slabs and 12" × 18" beams and 5" thick partition walls along all column lines. Floor loads also include working FF = 30 psf, RW = 50 psf, LL = 40 psf.

(i) Design the central column C1, if it is subjected to axial force only [i.e., no moments].

(ii) Use the section of (i) to check if it is adequate for C2 (subjected to axial force and working Mx = 20 k-ft) [Given: $f_c' = 3$ ksi, $f_y = 60$ ksi].

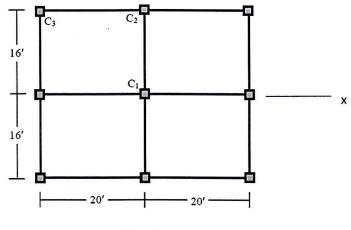


Fig: 4

5. Using USD method, for a square column footing

i. Estimate footing size and factored net soil pressure

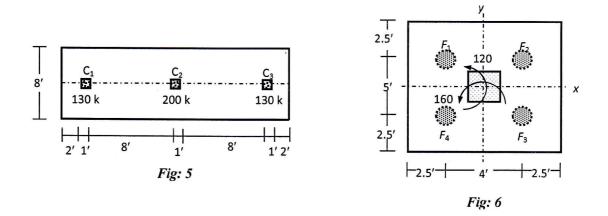
ii. Check the thickness for punching and beam shear.

iii. Design the reinforcement.

Given DL=350 k, LL= 270 k, f_c 'for footing = 3 ksi, f_c 'for column = 4.5 ksi , f_y =60 ksi, Depth of foundation= 5ft, column size= 18"x18", q_{all} = 6 ksf, γ_c =150 lb/ft³, γ_s =120 lb/ft³. 6. The loads (including self-weight) and arrangement of columns of size 12"x12" of the combined footing are shown in *Fig: 5*. Use WSD to

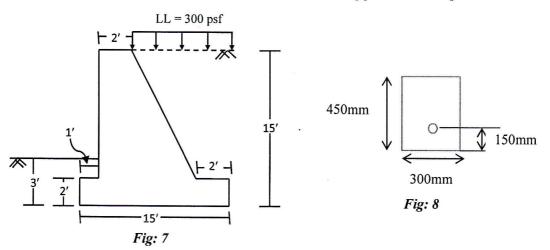
i. Draw the bending moment diagram of the footing.

ii. If the thickness of the footing is 25", check the adequacy of the thickness for punching shear, beam shear and bending.



- 7. Refer to the *Fig:* 6, A 24"×24" column carrying working loads of DL = 300 k, and LL = 180 k is underlain by soil with allowable bearing capacity = 2 ksf. The column also carries biaxial moments (due to LL) of M_x = 120 k-ft and M_y = 160 k-ft. Design the pile foundation by WSD method. [Given: f_c' =3 ksi, f_y =50 ksi, α_2 =0.8].
- Check the thickness and calculate the necessary reinforcements (Using USD method) for a 7'x12' rectangular footing having thickness of 28"and supporting a 16"x16" column with working loads of P_{DL}=170 k and P_{LL}=130 k [Given, f_c'=3 ksi, f_y=50 ksi, f_s=20 ksi, k=0.378, j=0.874, R_u=0.739 ksi].
- 9. A section of a gravity retaining wall as shown in *Fig:* 7was made to support the soil behind the wall and the surcharge on the ground surface. Check the external stability of the section against sliding and overturning. Also check the soil pressure under the base.

[Given, $\gamma_s = 120 \text{ pcf}, \phi = 30^\circ, f_{base} = 0.5$, Allowable bearing pressure= 3 tsf.]



10. A simply supported prestressed-concrete beam with a midspan section of 300 mm×450 mm (*Fig: 8*) has a simple span of 8 m and is loaded by a uniform load of 35 kN/m including its own weight. The prestressing tendon is located as shown in the *Fig: 8* and it produces an effective prestress of 2250 KN. Using the first concept of prestress concrete find out the fiber stresses at the midspan section.

PART B

[There are 5 (five) questions. Answer any 3 (Three)]

- 11. (a) (a) Briefly outline the design provisions for two types of shear reinforcement in flat slabs.(b) Mention and justify the maximum and minimum steel ratios specified by ACI for RC columns
- 12. (a) What is pre-stressed concrete? Compare prestressed concrete with reinforced concrete.(b) Write down the different name of losses that may occur in prestressed concrete.
- 13. (a) What is retaining wall? Name different types of retaining walls and explain their relative advantages.

14. (a) Outline the procedure for the structural design of piles and pile caps(b) Distinguish between allowable soil pressure and net soil pressure in the design of footings by USD.

15. (a) Define the band-width in placing reinforcements for rectangular footings and explain why it is used.

(b) Distinguish between active earth pressure and passive earth pressure.

⁽b) Mention the ACI recommendations for the size, spacing and arrangement of lateral ties and spirals.

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015 Program: B.Sc. Engineering (Civil)

Course Title: Design of Concrete Structures II Time: 3hrs

Course Code: CE 317 (B) Full Marks: 10x10=100

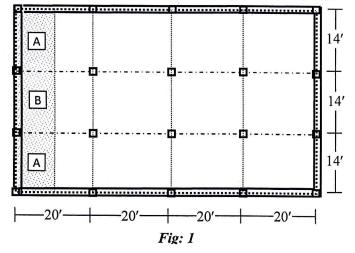
There are two parts of this question. (Part A and Part B)

PART A

[There are 9 (nine) questions. Answer any 7 (seven)] (All symbols have their usual meanings. Assume reasonable value for any missing data)

1. A building is to be designed as a flat plate structure (supported on edge beams). A plan of the building is shown in *Fig: 1*. The columns are 20"X20" in size. Use WSD method to calculate the column strip and middle strip moments of Panel A and Panel B.

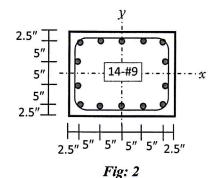
[Given, α_1 =3.66 and β_t = 1.45,FF = 30 psf, RW = 45psf, LL = 70psf, f_c' = 4 ksi, and f_y = 60 ksi].



2. For the tied column section shown below in *Fig: 2* [with $f_c'=3ksi, f_y=60 ksi$], use the WSD to i. Draw the interaction diagram about x-axis.

ii. Calculate the allowable moment of the section if it is subjected to axial force a. P = 150 k and b. P = 600 k

iii. Verify if the section is allowed to take P = 850 k, at an eccentricity $e = 4.5^{"}$.



3. A plan and section of a four storied building on beams and columns are shown in *Fig: 3*. All the beams in all floors are 12"X 20". Column sections are proposed to be 24"X 24"
5" wall along the peripherical beam Lime concrete on roof = 25 psf
Floor finish on each floor = 30 psf
Random wall load on each floor = 30 psf
Live load on each floor =60 psf
Live load on roof = 30 psf
Material properties: f_c' = 4 ksi, f_y = 60 ksi and f_s=24 ksi. Using U.S.D, design the edge column C₁.

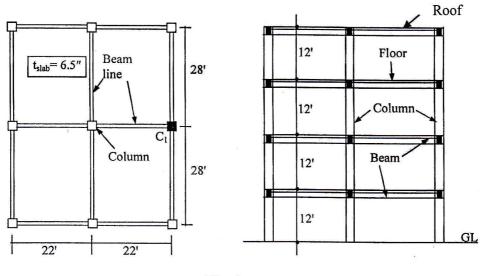
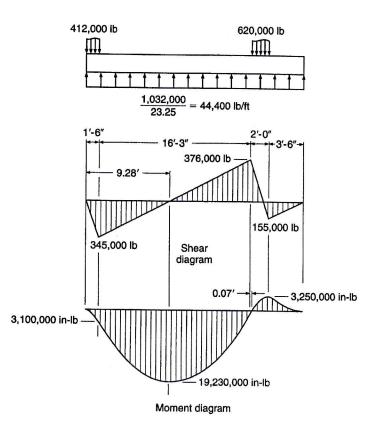


Fig: 3

- 4. Using USD Design a short square column for the following conditions: $P_u = 600 \text{ k}, M_u = 80 \text{ kf-ft}, f_c' = 4 \text{ ksi}, f_y = 60 \text{ ksi}$. Place bars uniformly around all four faces of the column.
- 5. A column 18 inch square, with $f_c = 4$ ksi, reinforced with eight #8 bars of $f_y = 60$ ksi, supports a dead load of 230 kips and live load of 180 kips. The allowable soil pressure qa is 5 kips/ft2. Design a square footing with base 5 ft below grade, use $f_c = 4$ ksi, $f_y = 60$ ksi.
- 6. An exterior 24 x 18 inch column with DL = 170 kips, LL=130 kips, and an interior 24 x 24 inch column with DL=250 kips, L = 200 kips are to be supported on a combined rectangular footing whose outer end cannot protrude beyond the outer face of the exterior column. The distance center to center of column is 18 ft and the allowable bearing pressure of the soil is 6 ksf. The bottom of the footing is 6 ft below grade and a surcharge of 100 psf is specified on the surface. Determine the thickness of the footing using the shear force and bending moment as shown *Fig: 4*, for f_c = 3 ksi, f_y = 60 ksi.



7. A 25x25 inch column (*Fig: 5*) carrying working loads DL = 300 k, and LL = 200 k is underlain by soil with allowable bearing capacity = 2 ksf. The column also carries biaxial moments (due to LL) of M_x = 100 k-ft and M_y = 200 k-ft. The footing area beneath the column must not exceed (10'x 10') because of proximity to adjacent columns. Use the USD to analyze and design the footing [Given: f_c '= 3 ksi, f_y = 50 ksi].

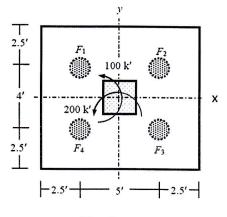


Fig: 5

8. A gravity wall shown in (*Fig: 6*) is to retain a bank 11.5 ft high whose horizontal surface is subject to live load surcharge of 500 psf. The soil is stiff clay and the allowable bearing capacity is 8.5 ksf. Determine whether the retaining wall is safe against overturning.

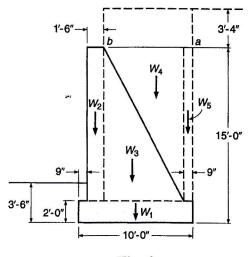


Fig: 6

9. A simply supported symmetrical I beam shown in *Fig:* 7 will be used on a 40 ft span. It has to carry live load of 0.75 kips/ft. The beam will be pretensioned with multiple seven-wire strands with the centroid at a constant eccentricity of 7.91 in. The prestressing force immediately after transfer will be 158 kips, after losses the force will be 134 kips. The specified $f_c' = 5000$ psi, and at the time of prstressing $f_{ci}' = 3750$. It has the following properties:

Moment of Inertia: $12,000 \text{ in}^4$ Concrete area: 176 in^2 Radius of gyration: $r^2 = 68.2 \text{ in}^2$ Section modulus: 1000 in^3 Self-weight: 0.183 kip/ft

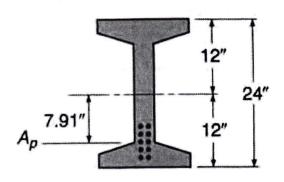


Fig: 7

PART B

[There are 5 (five) questions. Answer any 3 (Three)]

10. (a) Briefly outline the design provisions for two types of shear reinforcement in flat slabs.

(b) Mention and justify the maximum and minimum steel ratios specified by ACI for RC columns

(c) Explain why punching shear is considered in the design of column footings but not for wall footings.

(d) Distinguish between earth pressure at rest, active earth pressure and passive earth pressure.

(e) Mention the advantages and disadvantages of pre-stressed concrete compared to reinforced concrete.

List of Useful Formulae for CE 317

Column-Supported Slabs

*Total Static Moment at Factored Loads, $M_0 = w_n L_2 L_n^2/8$

* Total static moment for interior spans: $M_u^{(-)} = 0.65 M_0$, $M_u^{(+)} = 0.35 M_0$

* Distribution Factors applied to Static Moment M_0 for Positive and Negative Moments

Position of	Ext Edge	Slab with beams	No beam betw suppo	Exterior Edge fully	
Moment	unrestrained (a)	between all supports (b)	Without edge beam (c)	With edge beam (d)	restrained (e)
Exterior $M^{(-)}$	0.00	0.16	0.26	0.30	0.65
Interior $M^{(-)}$	0.75	0.70	0.70	0.70	0.65
$M^{(+)}$.	0.63	0.57	0.52	0.50	0.36

* $\alpha = E_{cb}I_b/E_{cs}I_s$ * $\beta_t = E_{cb}C/2E_{cs}I_s$ * $C = \sum (1-0.63 x/y) x^3 y/3$

% of Exterior $M^{(-)}$ supported by Column Strip = 100 -10 β_t + 12 $\beta_t (\alpha_l L_2/L_l) (1-L_2/L_l)$

% of $M^{(+)}$ supported by Column Strip = 60 + 30 ($\alpha_1 L_2/L_1$) (1.5- L_2/L_1)

% of Interior $M^{(-)}$ supported by Column Strip = 75 + 30 ($\alpha_1 L_2/L_1$) (1- L_2/L_1)

 $A_{\nu} = (V_n - V_c)/(f_{\nu} \sin \alpha)$ $S = A_{\nu}f_{\nu} d/(V - V_c)$

 $*V_c = 4\sqrt{f'_c b_o d} * V_c = (2 + 4/\beta_c)\sqrt{f'_c b_o d} * V_c = (2 + \alpha_s d/b_o)\sqrt{f'_c b_o d}$ [Use half of the values for WSD]

Short Column

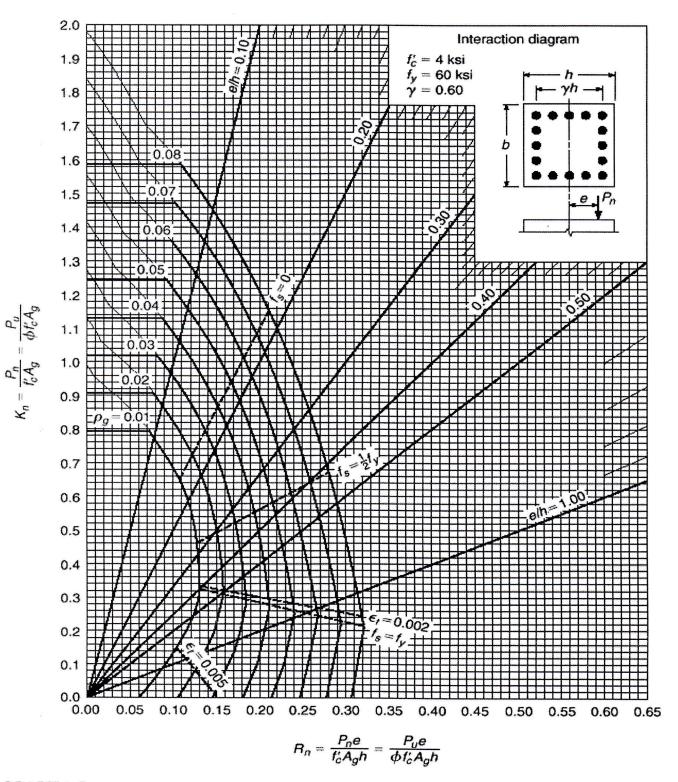
 $\begin{aligned} &*P_n = 0.85f_c A_c + f_y A_s = A_g \left[0.85f_c' + \rho_s \left(f_y - 0.85f_c' \right) \right] & *P_u = \alpha \, \phi A_g \left[0.85f_c' + \rho_s \left(f_y - 0.85f_c' \right) \right] \\ &*P_{all} = \phi' \left(0.25f_c A_g + f_{sall} A_s \right) = \phi' A_g (0.25f_c' + \rho_s f_{sall}) \\ &*P_r (P_a) + M/(M_f) = 1 \\ &*P_a = 0.34 f'_c (1 + \rho_g m) A_g \\ &*For symmetrical tied columns, \\ &M_o = 0.40 A_s f_y (d - d') \\ &and e_b = (0.17 + 0.67\rho_g m) d \\ &*For spiral columns, \\ &M_o = 0.12 A_{sTotal} f_y (D_s) \\ &and e_b = (0.14 + 0.43\rho_g m) d \\ &*P/(P_a) + M_x (M_{fx}) + M_y (M_{fy}) \leq 1 \\ &*1/P_{xy} = 1/P_x + 1/P_y - 1/P_0 \end{aligned}$

Footing and Foundation:

 $\begin{aligned} &*q_{nu} = (1.4 \ DL + 1.7 \ LL)/A_{(provided)} &*V_{fu} = q_{nu} \times tributary \ area & *v_{fu} = V_{fu}/bd & *v_{fu} = 2\phi \ \sqrt{f'_c} \\ &* V_{pu} = factored \ load \ -q_{nu} \times tributary \ area & *v_{pu} = V_{fu}/b_od & *v_{pu(all)} = 4\phi \ \sqrt{f'_c} \\ &* A_s = (f_c/f_y) \left[1 - \sqrt{\{1 - 2M_u/(\phi f_c \ bd^2)\}}\right] \ bd & *v_{f(all)} = 1.1 \ \sqrt{f'_c} & *v_{p(all)} = 2\phi \ \sqrt{f'_c} \\ &* Ru = \phi_{max}f_y [1 - 0.59\rho_{max} \cdot (f_y/f'_c)] \ R = 0.5f_c kj & *\rho_{max} = 0.75 \times 0.85 \times \beta_l \times (f'_c/f_y) \times [87/(87 + f_y)] \\ &* F(x, y) = P/N + M_x \ y/(\sum x_i^2) + M_y \ x/(\sum y_i^2) & *F = \phi \ (a_p \ f_{call} + a_s \ f_{sall}) & *L_p = F/\{\alpha_2 \ \tau_s(\pi d_p)\} \\ &* a_s = (P/\phi - a_p \ f_{call})/f_{sall} & *S_l = (100/0.2)(a_l/a_p)\pi d_c \end{aligned}$

<u>Retaining Wall:</u> *Y= h^2 + 3hh'/3(h+2h') * $P_a = 0.5[\{k_a\gamma_sh' + k_a\gamma_s(h'+h)\}] \times h$ *a) If Rv is in the middle third $q_1=(4l-6a)Rv/l^2$ $q_2=(6a-2l)Rv/l^2$ *b) If Rv is at the edge of middle third $q_1=2Rv/l$ *c) If Rv is at the edge, outside of middle third $q_1=2Rv/3a$.

Prestressed Concrete: $f = -(F/A_g) \pm (Fey/I)$ $f = -(F/A) \pm (Fey/I) \pm (My/I)$



GRAPH A.5

Column strength interaction diagram for rectangular section with bars on four faces and $\cdot = 0.60$ (for instructional use only).

CE 317 Formulae 2

Footings

$$A_{\rm S} = 0.85 f_c / f_y [1 - \sqrt{(1 - 2M_n/(0.85 f_c b d^2))}] b d$$

Retaining wall

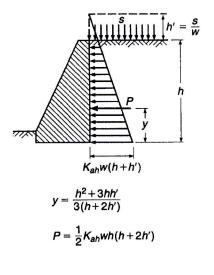
$$p_h = K_0 wh$$

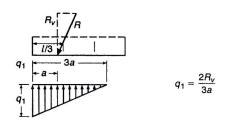
$$K_{ah} = \frac{1 - \sin \phi}{1 + \sin \phi} \qquad K_{ph} = \frac{1 + \sin \phi}{1 - \sin \phi}$$

Unit weights w, effective angles of internal friction ϕ , and coefficients of friction with concrete f

Soil	Unit Weight w, pcf	φ, deg	f
1. Sand or gravel without fine particles,			
highly permeable	110-120	33-40	0.5-0.6
2. Sand or gravel with silt mixture, low permeability	120-130	25-35	0.4-0.5
3. Silty sand, sand and gravel with high clay content	110-120	23-30	0.3-0.4
4. Medium or stiff clay	100-120	25-35ª	0.2-0.4
5. Soft clay, silt	90-110	20-25 ^a	0.2-0.3

" For saturated conditions, ϕ for clays and silts may be close to zero.





(c) Resultant outside middle third

Prestressed concrete

Permissible stresses in concrete in prestressed flexural members

	_	Class	
Condition	U	т	C*
a. Extreme fiber stress in compression immediately after transfer (except as in b)	$0.60 f_{ci}'$	$0.60f_{ci}^{\prime}$	$0.60 f'_{ci}$
b. Extreme fiber stress in compression at ends of simply supported members	$0.70 f_{ci}'$	$0.70 f_{ci}'$	$0.70 f'_{ci}$
c. Extreme fiber stress in tension immediately after transfer (except as in d)	$3\sqrt{f_{ci}'}$	$3\sqrt{f'_{ci}}$	$3\sqrt{f_{ci}'}$
d. Extreme fiber stress in tension immediately after transfer at the end of simply supported members [†]	$6\sqrt{f_{ci}'}$	$6\sqrt{f_{ci}'}$	$6\sqrt{f_{ci}'}$
e. Extreme fiber stress in compression due to prestress plus sustained load	$0.45f'_{c}$	$0.45f_{c}^{\prime}$	
f. Extreme fiber stress in compression due to prestress plus total load	$0.60 f_{c}'$	$0.60 f_{c}^{\prime}$	
g. Extreme fiber stress in tension f_i in precompressed tensile zone under service load	$\leq 7.5\sqrt{f_c'}$	$>7.5\sqrt{f_c'}$ and $\leq 12\sqrt{f_c'}$	

* There are no service stress requirements for Class C.

† When computed tensile stresses exceed these values, bonded auxiliary prestressed or nonprestressed reinforcement shall be provided in the tensile zone to resist the total tensile force in the concrete computed with the assumption of an uncracked section.

Top fibre stress
$$f_1 = -\frac{P_i}{A_c} + \frac{P_i e c_1}{I_c} = -\frac{P_i}{A_c} \left(1 - \frac{e c_1}{r^2}\right)$$

Bottom fibre stress $f_2 = -\frac{P_i}{A_c} - \frac{P_i e c_2}{I_c} = -\frac{P_i}{A_c} \left(1 + \frac{e c_2}{r^2}\right)$

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015 Program: B.Sc. Engineering (Civil)

Course Title: Environmental Engineering II Time: 3.0 hours

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Course No: CE 333 Full Marks: 150

Use <u>separate</u> scripts for each section. Answer any <u>three</u> out of <u>four</u> questions from each section (25*6=150) Assume reasonable value of missing data (if any)

Section A

1. (a	health education with figure.Make a comparison in a tabulated form between separate system and combined	[10] [15]
2. (a	sequence including the concept of water reclamation and reuse.	[5] [20]
3. (a	plumbing system.	[10] [15]
4. (a (l		[5] [20]
	Section B	
5. (a	disposal.	[10] [15]
6. (a	justify the statement.	[5] [20]

7.	(a)	Discuss the basic elements of VIP latrines with neat sketch.						[10]				
	(b)	Discuss	the	economic	considerations	of	small	bore	sewerage	system	over	

Page 1 of 2

- 8. (a) What basic processes are involved in the "Waste Stabilization Pond" method of wastewater treatment?
 - (b) Design a waste stabilization pond system to treat wastewater from a low-income settlement with a population of 25,000. The average wastewater flow is about 100 lpcd and the BOD contribution is 50 gm/person/day. The mean temperatures at winter season and summer season are 18°C and 29°C, respectively. Assume fecal coliform concentration in raw wastewater to be 1*10⁸/100 mL. It is desired that the final effluent be used for crop irrigation.

[20]

[15]

[5]

Temperature (°C)	Volumetric loading rate (g BOD/m ³ day)	BOD removal (%)
20	300	60
21	300	62
22	300	64
23	300	66
24	300	68
>25	300	70

Table-1: Design values of λ_{v} and BOD removal rate at various temperatures

Temperature (°C)	Surface loading rate (kgBOD/ha.day)	Temperature (°C)	Surface loading rate (kgBOD/ha.day)
16	183	23	311
17	199	24	331
18	217	25	350
19	235	26	369
20	253	27	389
21	272	28	406
22	292	29	424

$$N_{e} = N_{i} / (1 + K_{i} \theta_{a}) (1 + K_{i} \theta_{f}) (1 + K_{i} \theta_{m})$$
$$\theta_{m} = \left\{ \left[N_{i} / N_{e} (1 + K_{t} \theta_{a}) (1 + K_{t} \theta_{f}) \right]_{n}^{1} - 1 \right\} / K_{t}$$

University of Asia pacific **Department of Civil Engineering Final Examination Fall 2015** Program: B.Sc. Engineering (Civil)

Course Title: Transportation Engineering I (Transport and Traffic Design) Course Code: CE 351 Time: 3 Hours Full Marks: 150

There are six questions. Answer five of them

- 1. a) Name the types of signal controller.
 - Classify traffic signs along with brief description. b)
 - Two straight sections of a highway meet at an angle of 150° . If the radius of simple c) circular curve is 700m, find
 - i) Tangent distance
 - Length of long chord ii)
 - Mid-ordinate and iii)
 - Apex distance iv)
- 2. a) What are the objectives of traffic volume study?
 - What are the different types/ techniques of traffic calming? Explain any one of the types. b) 12
 - Spot speeds of 8 vehicles traversing 4 km segment of a highway are given below. c) 10 Calculate the Time Mean Speed and the Space Mean Speed of the vehicles.

Vehicle	Speed (km/hr.)
1	75
2	55
3	66
4	42
5	52
6	60
7	70
8	68

- Compare on-street and off-street parking. 3. a)
 - b) The following spot speeds (km/hr) were observed for 40 vehicles traversing a segment of 20 a highway.

25, 48, 56, 71, 66, 58, 48, 47, 53, 68, 29, 36, 59, 43, 45, 63, 46 42, 76, 45, 38, 65, 58, 34, 36, 53, 45, 73, 55, 43, 37, 47, 44, 68, 52, 57, 62, 65, 35, 39. Calculate the design speed, average speed, safe speed, median speed and lower limit of speed. (Consider pace as 10-19, 20-29 and so on)

Write short notes on any four: 4. a) i)

iii)

- ii) Origin Destination survey
- Forced flow v)
- Color vision Park and Ride system iv)

Visual acuity

b) A horizontal curve with a radius of 700 ft is designed for a two-lane highway having 14

16

10

6

12

12

8

a design speed of 75 mph. If the section of highway is having a 4% downgrade and coefficient of friction is 0.348, determine the smallest possible distance of any object can be placed from the centerline of the inside lane of the curve. Assume PR time 2.5.

- 5. a) A negative 4% grade vertical curve is followed by a positive 6% grade at a section of a 12 two-lane highway. What is the required length of vertical curve needed to satisfy design stopping sight distance? Assume the stopping sight distance to be 600 ft.
 - b) An arterial road has a design speed of 80 m/hr. There is a 3% grade (upgrade). What safe 12 stopping sight distance must be provided? Assume reaction time as 3 second and friction factor as .35.

6

- c) Define mobility and accessibility in terms of highway classification.
- 6. a) Briefly describe how Geographic factor and Political factor effect the development of 15 transportation system in Bangladesh.
 - b) Briefly explain the constraints of road and rail transportation sector in Bangladesh.

Necessary equations: $L = \frac{AS^2}{100(\sqrt{2h_1} + \sqrt{2h_2})^2}$ S<L: $L = 2S - \frac{200(\sqrt{h_1} + \sqrt{h_2})^2}{A}$ S>L: $L = \frac{AS^2}{200[2.0 + S(\tan 1^\circ)]}$ S<L: S>L: $L = 2S - \frac{200[2.0 + S(\tan 1^{\circ})]}{\Delta}$

University of Asia Pacific Department of Civil Engineering Final Examination Fall 2015 Program: B. Sc. Engineering (Civil)

Course Code: CE 363 Full Marks: 150 Course Title: Engineering Hydrology Time: 3 hours

There are TWO sections in the question paper namely "Part A" and "Part B". You have to answer from the both sections according to the instruction mentioned on each section.

		There are FOI	R questions	Part A	THDEE (3	* 25 - 75)	
			JIX questions	s answer any	TIINEE (S	23 - 73)	
1. (a) Wr	ite sl	nort notes on:					()
	i.	Weather front		iii. Vapor p	ressure		
	ii.	Residence time	e	iv. Pan co-	efficient		
1. (b) De	scrib	e the procedure	to estimate p	recipitable wa	ter from a s	tatic atmospher	ricair (1
column.							
1. (c) A c	atch	ment area has 6	rain gauge st	ations. In a ye	ar the annua	l rainfall record	ded by (
		e as follows:	00				
Station	A	В	С	D	Е	F	
Rainfall	78.	3 85.7	105.1	110.9	95.0	72.8	
For a 129	% err	or in the estimat	tion of the me	ean rainfall, ca	lculate the o	optimum numb	er of
		17 1 7 1 1				· · · · · · · · · · · · · · · · · · ·	

stations required to be established in the catchment.

2. (a) There were 6 rain gauge stations namely N, O, P, Q, R, and S where station P was (5) inoperative for the month. At that month rainfall recorded in the other five stations were 6.2, 9.1, 5.9, 8.3, 5.7 cm respectively. If the average annual rainfalls for the stations are 91, 67, 75, 86, 69, 72 cm. Estimate rainfall at station P for that month.

2. (b) Annual rainfall data are available below for four gauges (E, F, G, H). Gauge H was (15) relocated permanently at the end of 1987. Therefore rainfall data for gauge H for the period 1985-1987 must be adjusted to the rainfall characteristics at the new location. Find adjusted rainfall data at H.

Year		Annual Ra	ainfall (in)	
Γ	Е	F	G	Н
1985	22	26	23	28
1986	21	26	25	33
1987	27	31	28	38
1988	25	29	29	31
1989	19	22	23	24
1990	24	25	26	28
1991	17	19	20	22
1992	21	22	23	26

Page	1	of	4	
* ~ De	-	O.		

2. (c) What are the factors	affecting I	Evapotrans	spiration?			(5)			
3. (a) Describe different me	ethods of l	base flow	separation			(10)			
3. (b) For a drainage basin data:	of 575 km	² , isohyet	als drawn	for a storn	n gave the foll	lowing (8)			
Isohyetal intervals (cm)	15-12	12-9	9-6	6-3	3-1				
Inter Isohyetal area (km ²)	92	128	120	175	85				
Estimate the average depth	Estimate the average depth of precipitation over the catchment.								
3. (c) Discuss how the role shape of flood hydrograph.		pe, slope	and draina	ge density	of a basin aff	fects the (7)			
4. (a) Explain the following	g:					(9)			
i. Conditions that must be present for the production of precipitation.									
ii. Initial loss to reduce the water volume available for runoff.									
iii. Intensity-du	ration-free	quency cu	rve						

4. (b) A storm with 15 cm precipitation produced a direct runoff of 7.8 cm. The time (10) distribution of the storm is as follows. Estimate Φ index of the storm.

time from start (hr)	1	2	3	4	5	6	7	8
Incremental rainfall (cm)	0.6	1.35	2.25	3.45	2.7	2.4	1.5	0.75

4. (c) Show different components of hydrograph in a neat sketch.

(6)

Ther	e are F	OUR o	questic		rt <u>B</u> wer an	THRE	E (3	* 25 =	75)	
5. (a) Write a shor	t note o	n runoi	ff char	acterist	ics of st	reams w	ith neat	sketch	es.	
5. (b) The ordinate	es of a 4	-h unit	hydro	graph a	re as gi	ven belo	w:			
Time	0	2 4			-			16	5	18
ordinates of 4-hr UH (cumec)	0	24 4	9 82	12	2 15	5 110) 89	58	2 4	34
If two storms, each respectively, then cm ER rain.	1 of 4 - h	r durati	ion and	l having	g rainfal	l excess	values o	of 3-cm	n and	4-cm
5. (c) What are the reservoir routing?	climat	ic facto	ors affe	cting fl	ood hyd	lrograph	? What o	lata ar	e requ	ired for
6. (a) Describe the	metho	ds of de	evelop	ing unit	t hydrog	raph of	different	durati	ons.	
6. (b) The followin 720 km ² due to a 6	-hr rain	fall. Do	erive tl	he ordir	nates of					
Time 6 12	2 18	24	30 405	36 350	42	48 54 05 14:		66 70	72 50	78 42
Time 6 12 Discharge 40 64 7. (a) A basin has $C_p = 0.65$. Develop 7. (b) Describe the 7. (c) An area of 12 rational method fo 8. (a) Describe the Gumbel's method. 8. (b) The followin	2 18 2 215 480 sq. p a 6-hr p proced 2 acres r a 1.75 proced	24 360 km of synthe lure of has a r inch p lure of	30 405 area, L tic uni estima unoff c er hou estima	36 350 z= 40 kr t hydro ting 'k' co-effic r rainfa ting flo d for a	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od discl	$\frac{05}{14} = 16 \text{ k}$ or this ba in Mush 0.55. Fin ity. harge of de stream	5 100 cm. Assu isin usin kingum o d peak d any inte	70 uming g Snyc equatio ischar; rval us	50 $C_t = 1.$ der's r on. ge usi ing	42 2 and nethod.
Discharge 40 64 7. (a) A basin has $C_p = 0.65$. Develop 7. (b) Describe the 7. (c) An area of 12 rational method fo 8. (a) Describe the Gumbel's method. 8. (b) The followin rating equation of Compute the disch	2 18 2 215 480 sq. p a 6-hr p roced 2 acres r a 1.75 proced ng data the curn narge.	24 360 km of synthe lure of has a r inch p lure of were content me	30 405 area, L tic uni estima unoff o er hou estima ollecte ter is V	36 350 $z = 40 km$ t hydro ting 'k' co-effic r rainfa ting flo d for a $V = 0.33$	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od disch 24 m with $N_s + 0.0$	$\frac{05}{14} = 16 \text{ k}$ or this ba in Mush 0.55. Find ity. harge of de stream 05 m/s.	5 100 cm. Assu isin usin kingum o d peak d any inter m at a ga	70 uming g Snyc equatio ischar; rval us	50 $C_t = 1.$ der's r on. ge usi sing statio	42 2 and nethod. ng n. The
Time612Discharge40647. (a) A basin hasCpCp0.65. Develop7. (b) Describe the7. (c) An area of 12rational method fo8. (a) Describe theGumbel's method.8. (b) The followinrating equation ofCompute the dischDistance from left	2 18 2 215 480 sq. p a 6-hr p roced 2 acres r a 1.75 proced ng data the curn narge.	24 360 km of synthe lure of has a r inch p lure of were content me	30 405 area, L tic uni estima unoff o er hou estima ollecte ter is V	36 350 $z = 40 km$ t hydro ting 'k' co-effic r rainfa ting flo d for a $V = 0.33$	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od disch 24 m wit $N_s + 0.0$ 2	$\frac{05 14}{16}$ $\frac{16}{16}$	5 100 cm. Assu isin usin kingum o d peak d any inte m at a ga 6	70 ming g Snyc equatio ischar; rval us auging	$\frac{50}{C_t=1.}$ der's r on. ge usi sing statio	42 2 and nethod. ng n. The 12
Time 6 12 Discharge 40 64 7. (a) A basin has 6 C _p = 0.65. Develop 7. (b) Describe the 7. (c) An area of 12 rational method fo 8. (a) Describe the Gumbel's method. 8. (b) The followin rating equation of Compute the disch Distance from left Depth (m)	2 18 2 215 480 sq. p a 6-hr p a 6-hr p proced 2 acres r a 1.75 proced ng data the curn arge. water e	24 360 km of synthe lure of has a r inch p lure of were co rent me	30 405 area, L tic uni estima unoff c er hou estima ollecte ter is v	36 350 $z = 40 km$ t hydro ting 'k' co-effic r rainfa ting flo d for a $V = 0.33$	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od disch 24 m with $N_s + 0.0$	$\frac{05}{14} = 16 \text{ k}$ or this ba in Mush 0.55. Find ity. harge of de stream 05 m/s.	5 100 cm. Assu isin usin kingum o d peak d any inter m at a ga	70 uming g Snyc equatio ischar; rval us auging	50 $C_t = 1.$ der's r on. ge usi sing statio	42 2 and nethod. ng n. The
Time 6 12 Discharge 40 64 7. (a) A basin has C p = 0.65. Develop 7. (b) Describe the 7. (c) An area of 12 rational method fo 8. (a) Describe the Gumbel's method. 8. (b) The followin rating equation of Compute the disch Distance from left Depth (m) Revolution per sec	2 18 215 480 sq. p a 6-hr p a 6-hr p roced 2 acres r a 1.75 proced ng data the curn arge. water e	24 360 km of synthe lure of has a r inch p lure of were co rent me edge (n 0.6 dep	30 405 area, L tic uni estima unoff c er hou estima ollecte ter is v n) th	36 350 $z = 40 km$ t hydro ting 'k' co-effic r rainfa ting flo d for a $V = 0.33$ 0 0 0	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od disch 24 m wi $N_s + 0.0$ 2 0.5 0.43	$\frac{05 14}{1.1}$	5 100 tm. Assu usin usin kingum o d peak d any inter m at a ga 6 1.95 1.10	70 ming g Snyc equationischar; rval us auging 2. 1	50 $C_t = 1.$ der's r on. ge usi ing statio 9 .25 .17	42 2 and nethod. ng n. The 12 1.85 1.00
Time 6 12 Discharge 40 64 7. (a) A basin has 6 C _p = 0.65. Develop 7. (b) Describe the 7. (c) An area of 12 rational method fo 8. (a) Describe the Gumbel's method. 8. (b) The followin rating equation of Compute the disch Distance from left Depth (m)	2 18 215 480 sq. p a 6-hr p a 6-hr p roced 2 acres r a 1.75 proced ng data the curn arge. water e	24 360 km of synthe lure of has a r inch p lure of were co rent me edge (n 0.6 dep	30 405 area, L tic uni estima unoff c er hou estima ollecte ter is v	36 350 $z = 40 km$ t hydro ting 'k' co-effic r rainfa ting flo d for a $V = 0.33$ 0 0 0	42 470 2 m and L graph fo and 'x' ient of 0 11 intens od disch 24 m with $N_s + 0.0$ 2 0.5	$\frac{05 14}{1.1}$ $\frac{05 14}{1.1}$ $\frac{05 14}{1.1}$ $\frac{05 14}{1.1}$	5 100 cm. Assu isin usin kingum o d peak d any inte m at a ga 6 1.95	70 iming g Snyc equationischary rval us auging 2 1 2	50 $C_t = 1.$ der's r on. ge usi ing statio 9 .25 .17	42 2 and nethod. ng n. The 12 1.85

Page 3 of 4

8. (c) The inflow hydrograph readings for a channel reach are given for which the (10) Muskingum coefficients of k=28 hr and x=0.35. Route the flood through the reach and determine the attenuation and time lag of outflow. Outflow at the beginning of the flood may be taken as the same as inflow.

Time (hr)	0	6	12	18	24	30	36	42	48
Inflow (cumec)	15	16	31	96	121	102	85	70	57
Time (hr)	54	60	66	72	78				
Inflow (cumec)	47	35	26	22	17				